

Fixing the Flux: a Dual Approach to Computing Transport Coefficients

Noé Blassel (joint work with Gabriel Stoltz)¹

CERMICS lab, École des Ponts ParisTech - MATHERIALS team, Inria

June 27, 2023



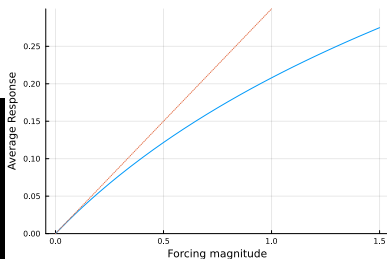
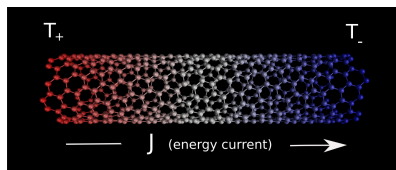
Inria



¹N. Blassel & G.Stoltz, (2023), ArXiv 2305.08224

Transport coefficients

- Measure sensitivity of flux induced by nonequilibrium perturbation
- Parametrize macroscopic evolution equations (e.g. Navier–Stokes)
- Dynamical quantities: thermal conductivity, mobility, shear viscosity...
- Magnitude of flux depends linearly on the flux in the small perturbation regime.
- Equilibrium methods (Green–Kubo, tangent dynamics², martingale product estimators³).
- Nonequilibrium dynamics.



²R. Assaraf, B. Jourdain, T. Lelièvre & R. Roux (2015)

³P. Pleháč, G. Stoltz & T. Wang (2021)

Standard NEMD dynamics: formal framework

Fix a d -dimensional configuration space \mathcal{X} , a reference drift b and diffusion matrix σ . External forcing: $F : \mathcal{X} \rightarrow \mathbb{R}^d$, modulated in strength by $\eta \in \mathbb{R}$. The response flux is a function $R : \mathcal{X} \rightarrow \mathbb{R}$, with zero average at equilibrium.

- Standard NEMD:

$$dX_t^\eta = b(X_t^\eta) dt + \sigma(X_t^\eta) dW_t + \eta F(X_t^\eta) dt.$$

Standard NEMD dynamics: formal framework

Fix a d -dimensional configuration space \mathcal{X} , a reference drift b and diffusion matrix σ . External forcing: $F : \mathcal{X} \rightarrow \mathbb{R}^d$, modulated in strength by $\eta \in \mathbb{R}$. The response flux is a function $R : \mathcal{X} \rightarrow \mathbb{R}$, with zero average at equilibrium.

- Standard NEMD:

$$dX_t^\eta = b(X_t^\eta) dt + \sigma(X_t^\eta) dW_t + \eta F(X_t^\eta) dt.$$

- We measure averages of the response, with respect to the invariant measure μ^η (typically using ergodic averages). See⁴ for precise $\exists!$ statements for μ^η .

⁴R. Spacek & G. Stoltz (2023)

Standard NEMD dynamics: formal framework

Fix a d -dimensional configuration space \mathcal{X} , a reference drift b and diffusion matrix σ . External forcing: $F : \mathcal{X} \rightarrow \mathbb{R}^d$, modulated in strength by $\eta \in \mathbb{R}$. The response flux is a function $R : \mathcal{X} \rightarrow \mathbb{R}$, with zero average at equilibrium.

- Standard NEMD:

$$dX_t^\eta = b(X_t^\eta) dt + \sigma(X_t^\eta) dW_t + \eta F(X_t^\eta) dt.$$

- We measure averages of the response, with respect to the invariant measure μ^η (typically using ergodic averages). See⁴ for precise $\exists!$ statements for μ^η .
- Transport coefficient:

$$\rho_{R,F} = \lim_{\eta \rightarrow 0} \frac{1}{\eta} \int_{\mathcal{X}} R d\mu^\eta, \quad \widehat{\rho}_{R,F}^{T,\eta} = \frac{1}{\eta T} \int_0^T R(X_t^\eta) dt$$

⁴R. Spacek & G. Stoltz (2023)

Standard NEMD dynamics: formal framework

Fix a d -dimensional configuration space \mathcal{X} , a reference drift b and diffusion matrix σ . External forcing: $F : \mathcal{X} \rightarrow \mathbb{R}^d$, modulated in strength by $\eta \in \mathbb{R}$. The response flux is a function $R : \mathcal{X} \rightarrow \mathbb{R}$, with zero average at equilibrium.

- Standard NEMD:

$$dX_t^\eta = b(X_t^\eta) dt + \sigma(X_t^\eta) dW_t + \eta F(X_t^\eta) dt.$$

- We measure averages of the response, with respect to the invariant measure μ^η (typically using ergodic averages). See⁴ for precise $\exists!$ statements for μ^η .
- Transport coefficient:

$$\rho_{R,F} = \lim_{\eta \rightarrow 0} \frac{1}{\eta} \int_{\mathcal{X}} R d\mu^\eta, \quad \widehat{\rho}_{R,F}^{T,\eta} = \frac{1}{\eta T} \int_0^T R(X_t^\eta) dt$$

- Challenging to estimate due to scaling of the variance in $O(\eta^{-2})$ for the standard estimator. Variance reduction techniques: active area of research⁵

⁴R. Spacek & G. Stoltz (2023)

⁵R. Spacek & G. Stoltz (2023), S. Darshan, A. Eberle & G. Stoltz (In preparation)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶
- Dual dynamics:

$$dY_t^r = b(Y_t^r) dt + \sigma(Y_t^r) dW_t + F(Y_t^r) d\Lambda_t^r.$$

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶
- Dual dynamics:

$$dY_t^r = b(Y_t^r) dt + \sigma(Y_t^r) dW_t + F(Y_t^r) d\Lambda_t^r.$$

- Stochastic process Λ_t^r chosen to fix the response: $R(Y_t^r) = r$ for all $t \geq 0$.

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶
- Dual dynamics:

$$dY_t^r = b(Y_t^r) dt + \sigma(Y_t^r) dW_t + F(Y_t^r) d\Lambda_t^r.$$

- Stochastic process Λ_t^r chosen to fix the response: $R(Y_t^r) = r$ for all $t \geq 0$.
- Dynamics on a submanifold $\Sigma_r = R^{-1}\{r\}$.

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶
- Dual dynamics:

$$dY_t^r = b(Y_t^r) dt + \sigma(Y_t^r) dW_t + F(Y_t^r) d\Lambda_t^r.$$

- Stochastic process Λ_t^r chosen to fix the response: $R(Y_t^r) = r$ for all $t \geq 0$.
- Dynamics on a submanifold $\Sigma_r = R^{-1}\{r\}$.
- Explicit form for the forcing:

$$\Lambda_t^r = \Lambda_0^r + \int_0^t \lambda(Y_s^r) ds + \int_0^t \tilde{\lambda}(Y_s^r) dW_s.$$

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶
- Dual dynamics:

$$dY_t^r = b(Y_t^r) dt + \sigma(Y_t^r) dW_t + F(Y_t^r) d\Lambda_t^r.$$

- Stochastic process Λ_t^r chosen to fix the response: $R(Y_t^r) = r$ for all $t \geq 0$.
- Dynamics on a submanifold $\Sigma_r = R^{-1}\{r\}$.
- Explicit form for the forcing:

$$\Lambda_t^r = \Lambda_0^r + \int_0^t \lambda(Y_s^r) ds + \int_0^t \tilde{\lambda}(Y_s^r) dW_s.$$

- Explicit form for the dynamics:

$$dY_t^r = \bar{P}_{F, \nabla R}(Y_t^r) [b(Y_t^r) dt + \sigma(Y_t^r) dW_t] - \frac{(\nabla^2 R : \Pi_{F, \nabla R, \sigma}) F}{2 \nabla R \cdot F}(Y_t^r) dt.$$

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...)

Dual approach: formal framewok

- Idea: fix value of the flux r exactly, measure average magnitude of the forcing needed to induce it. Stochastic version of the Norton method.⁶
- Dual dynamics:

$$dY_t^r = b(Y_t^r) dt + \sigma(Y_t^r) dW_t + F(Y_t^r) d\Lambda_t^r.$$


- Stochastic process Λ_t^r chosen to fix the response: $R(Y_t^r) = r$ for all $t \geq 0$.
- Dynamics on a submanifold $\Sigma_r = R^{-1}\{r\}$.
- Explicit form for the forcing:

$$\Lambda_t^r = \Lambda_0^r + \int_0^t \lambda(Y_s^r) ds + \int_0^t \tilde{\lambda}(Y_s^r) dW_s.$$

- Explicit form for the dynamics:

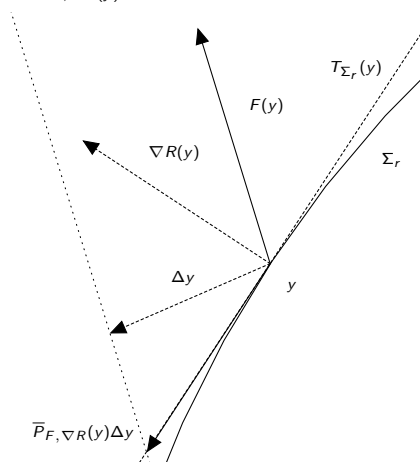
$$dY_t^r = \bar{P}_{F, \nabla R}(Y_t^r) [b(Y_t^r) dt + \sigma(Y_t^r) dW_t] - \frac{(\nabla^2 R : \Pi_{F, \nabla R, \sigma}) F}{2 \nabla R \cdot F}(Y_t^r) dt.$$

- $\bar{P}_{F, \nabla R}$ is a non-orthogonal projector onto $\nabla R^\perp = T\Sigma_r$ in the direction F .

⁶Evans, Hoover, Failor, Moran, & Ladd (1983), D. Evans, & G. Morris (1985, 1986, 1993, ...) 

Geometric picture

The oblique projector $\bar{P}_{F, \nabla R(y)}$:



$$\bar{P}_{F, \nabla R}(y) = \text{Id} - \frac{F(y) \otimes \nabla R(y)}{F(y) \cdot \nabla R(y)},$$

$$\Pi_{F, \nabla R, \sigma} = \bar{P}_{F, \nabla R} \sigma \sigma^T \bar{P}_{\nabla F, R}^T.$$

Dual transport coefficients

Assume $\exists!$ Norton steady-state $\mu^{r,*}$ for all r small enough.

- Average forcing magnitude determined by the bounded variation component of the forcing process

$$\int_0^t \lambda(Y_s^r) ds, \quad t \geq 0.$$

Dual transport coefficients

Assume $\exists!$ Norton steady-state $\mu^{r,*}$ for all r small enough.

- Average forcing magnitude determined by the bounded variation component of the forcing process

$$\int_0^t \lambda(Y_s^r) ds, \quad t \geq 0.$$

- Dual transport coefficient:

$$\rho_{R,F}^* = \lim_{r \rightarrow 0} \frac{r}{\int_{\Sigma_r} \lambda d\mu^{r,*}}, \quad \widehat{\rho}_{R,F}^{T,r,*} = \frac{Tr}{\int_0^T \lambda(Y_t^r) dt}.$$

Dual transport coefficients

Assume $\exists!$ Norton steady-state $\mu^{r,*}$ for all r small enough.

- Average forcing magnitude determined by the bounded variation component of the forcing process

$$\int_0^t \lambda(Y_s^r) ds, \quad t \geq 0.$$

- Dual transport coefficient:

$$\rho_{R,F}^* = \lim_{r \rightarrow 0} \frac{r}{\int_{\Sigma_r} \lambda d\mu^{r,*}}, \quad \widehat{\rho}_{R,F}^{T,r,*} = \frac{Tr}{\int_0^T \lambda(Y_t^r) dt}.$$

- The procedure can be generalized to vector-valued responses and time-dependent constraints.

Dual transport coefficients

Assume $\exists!$ Norton steady-state $\mu^{r,*}$ for all r small enough.

- Average forcing magnitude determined by the bounded variation component of the forcing process

$$\int_0^t \lambda(Y_s^r) ds, \quad t \geq 0.$$

- Dual transport coefficient:

$$\rho_{R,F}^* = \lim_{r \rightarrow 0} \frac{r}{\int_{\Sigma_r} \lambda d\mu^{r,*}}, \quad \widehat{\rho}_{R,F}^{T,r,*} = \frac{Tr}{\int_0^T \lambda(Y_t^r) dt}.$$

- The procedure can be generalized to vector-valued responses and time-dependent constraints.
- Nonequilibrium analog of microcanonical/canonical duality (equivalence of ensembles).

Norton Langevin dynamics

Apply the general framework to kinetic Langevin equations, with responses of the form

$$R(q, p) = p^\top G(q).$$

Typical examples: mobility, shear viscosity.

- NEMD:

$$\begin{cases} dq_t^\eta = M^{-1} p_t^\eta dt, \\ dp_t^\eta = [-\nabla V(q_t^\eta) + \eta F(q_t^\eta)] dt - \gamma M^{-1} p_t^\eta dt + \sqrt{\frac{2\gamma}{\beta}} dW_t. \end{cases} \quad (1)$$

M =mass matrix, $0 < \gamma$ =damping coefficient, $\beta = (k_B T)^{-1}$ =inverse temperature.

Norton Langevin dynamics

Apply the general framework to kinetic Langevin equations, with responses of the form

$$R(q, p) = p^T G(q).$$

Typical examples: mobility, shear viscosity.

- NEMD:

$$\begin{cases} dq_t^\eta = M^{-1} p_t^\eta dt, \\ dp_t^\eta = [-\nabla V(q_t^\eta) + \eta F(q_t^\eta)] dt - \gamma M^{-1} p_t^\eta dt + \sqrt{\frac{2\gamma}{\beta}} dW_t. \end{cases} \quad (1)$$

M =mass matrix, $0 < \gamma$ =damping coefficient, $\beta = (k_B T)^{-1}$ =inverse temperature.

- Norton:

$$\begin{cases} dq_t^r = M^{-1} p_t^r dt, \\ dp_t^r = \bar{P}_{F,G}(q_t^r) \left(-\nabla V(q_t^r) dt - \gamma M^{-1} p_t^r dt + \sqrt{\frac{2\gamma}{\beta}} dW_t \right) \\ \quad - \frac{\nabla G(q_t^r) p_t^r \cdot M^{-1} p_t^r}{F(q_t^r) \cdot G(q_t^r)} F(q_t^r) dt. \end{cases} \quad (2)$$

Example: mobility computations

Forcing: constant perturbation $F \in \mathbb{R}^{dN}$.

Example: mobility computations

Forcing: constant perturbation $F \in \mathbb{R}^{dN}$. Response: particle flux in the direction F

$$R = F^T M^{-1} p.$$

Example: mobility computations

Forcing: constant perturbation $F \in \mathbb{R}^{dN}$. Response: particle flux in the direction F

$$R = F^T M^{-1} p.$$

Single drift – singular forcing:

$$F_{i,x} = \delta_{i,1}, \quad F_{i,y} = F_{i,z} = 0$$

Color drift – bulk forcing:

$$F_{i,x} = (-1)^i N^{-1/2}, \quad F_{i,y} = F_{i,z} = 0$$

Norton mobility dynamics

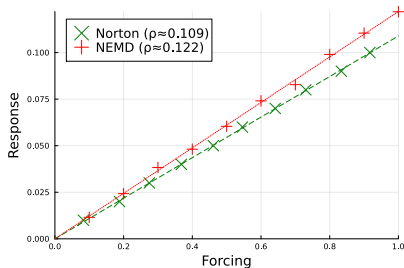
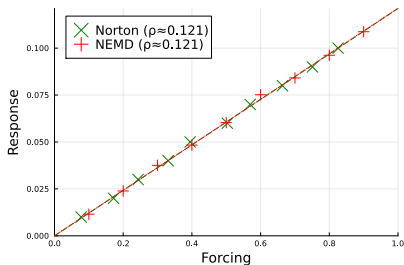
Projection of equilibrium momentum dynamics

$$\begin{cases} dq_t = M^{-1} p_t dt, \\ dp_t = \bar{P}_{F, M^{-1}F} \left(-\nabla V(q_t) dt - \gamma M^{-1} p_t dt + \sqrt{\frac{2\gamma}{\beta}} dW_t \right), \end{cases} \quad (3)$$

$$\bar{P}_{F, M^{-1}F} = \text{Id} - \frac{FF^T M^{-1}}{F^T M^{-1}F}.$$

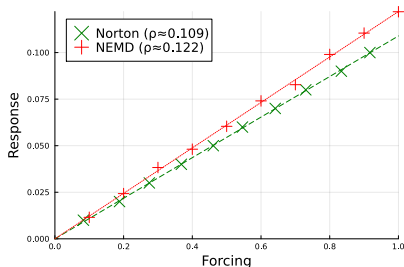
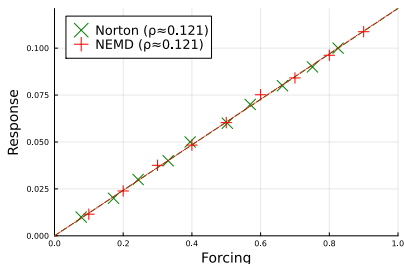
Numerical results: mobility

Lennard-Jones fluid of 1000 particles (liquid argon). Left: color drift (bulk forcing/response). Right: single drift (singular forcing/response).



Numerical results: mobility

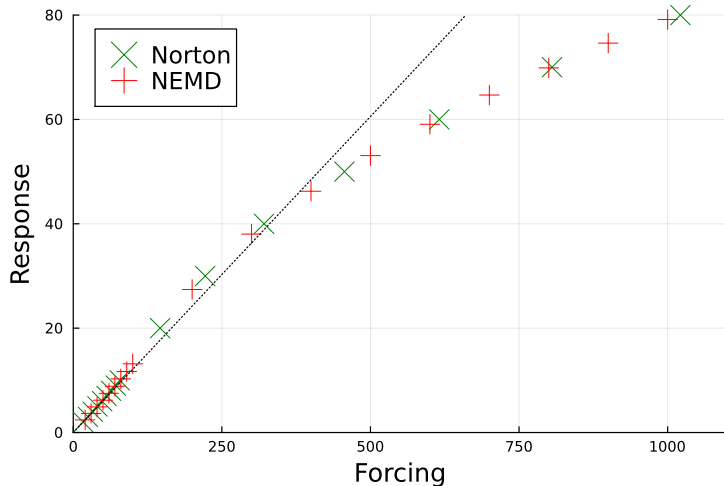
Lennard-Jones fluid of 1000 particles (liquid argon). Left: color drift (bulk forcing/response). Right: single drift (singular forcing/response).



Linear responses coincide in the case of bulk forcings.

Numerical results: mobility with a bulk forcing

Non-linear responses coincide as well:



Shear viscosity⁷

Forcing F acts only on x -components, according to a y -profile f .


$$\forall 1 \leq i \leq N, \forall 2 \leq \alpha \leq d, \quad F(q)_{i,x} = f(q_{i,y}), \quad F(q)_{i\alpha} = 0,$$

In non-equilibrium steady-state, measurable y -profile in the x -components of velocity. Localized linear response: $u_x(y)$. Shear viscosity ν :

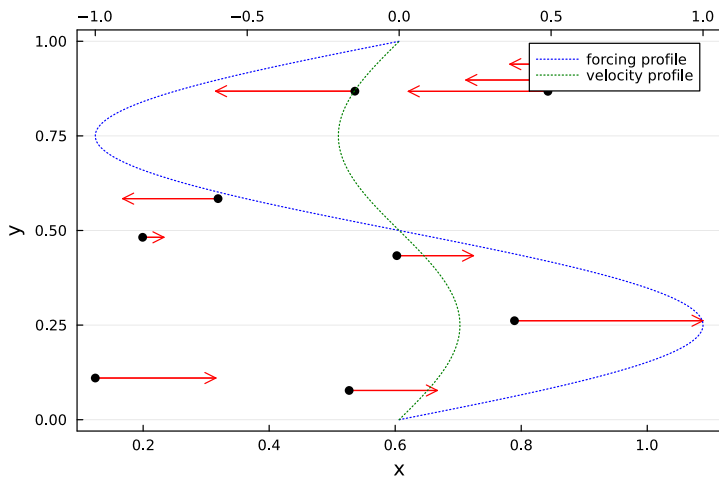
$$-\nu u_x''(y) + \gamma_x \rho u_x(y) = \rho f(y) \implies \nu = \rho \left(\frac{F_1}{U_1} - \gamma_x \right) \left(\frac{L_y}{2\pi} \right)^2,$$

Fourier coefficients F_1, U_1 of f and u_x . Response observable

$$R(q, p) = \frac{1}{N} \sum_{j=1}^N \left(M^{-1} p \right)_{j,x} \exp \left(\frac{2i\pi q_{j,y}}{L_y} \right). \quad (4)$$

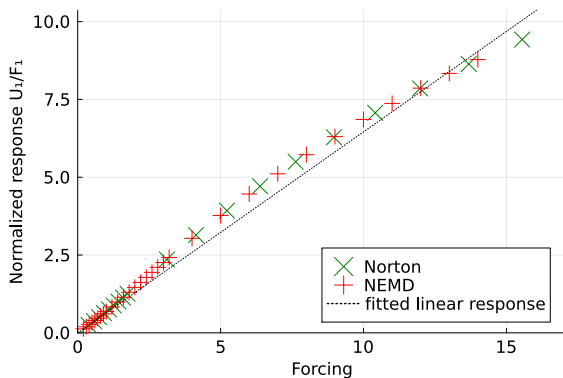
⁷G. Stoltz & R. Joubaud (2012), Gosling, McDonald & Singer (1973) 

Shear viscosity



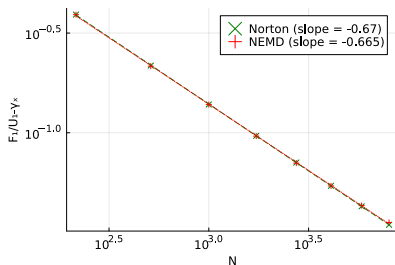
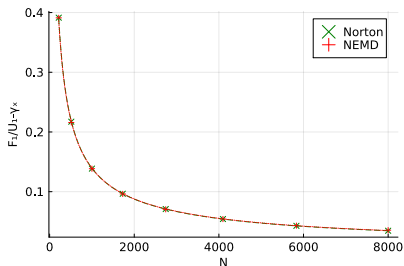
Shear viscosity: equivalence of nonlinear responses

Lennard–Jones fluid: consistent (non)linear response profiles:



Shear viscosity: consistency in the thermodynamic limit

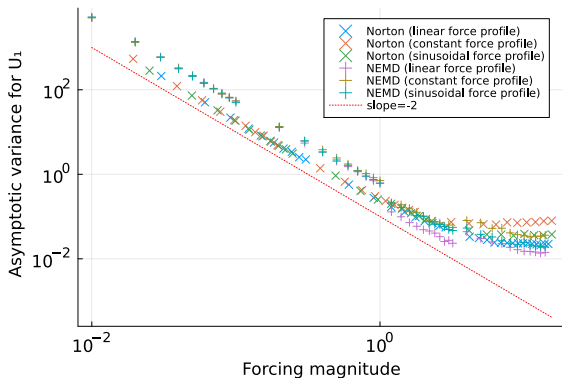
Ergodic estimators of the linear response are consistent results in the limit $N \rightarrow \infty$:



Extrapolating the estimated shear viscosity to the limit $N \rightarrow \infty$ give close estimates for NEMD and dual approach.

Shear viscosity: gain in asymptotic variance

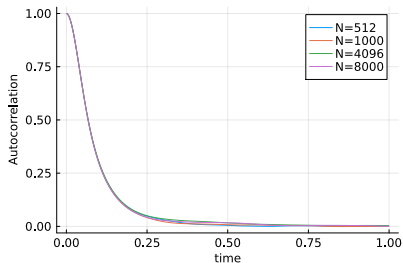
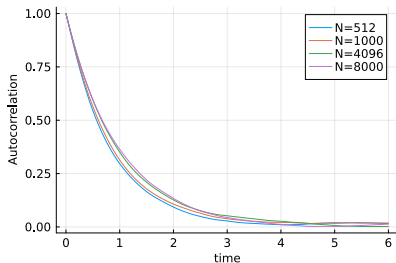
Asymptotic variance of estimators for F_1/U_1 from ergodic averages:



Standard NEMD \approx doubles the asymptotic variance with respect to dual approach.

Shear viscosity: decay of autocorrelations

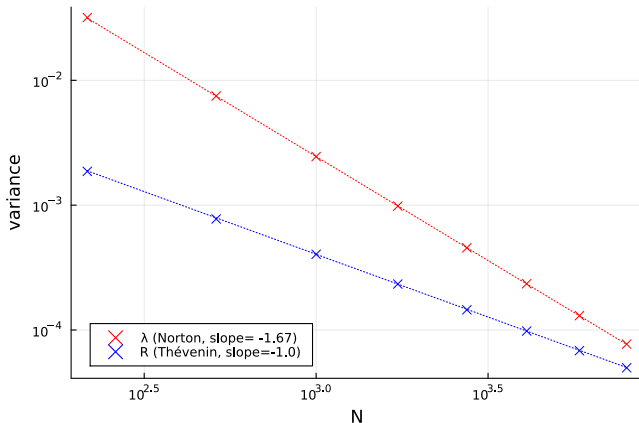
To explain this discrepancy, we compare the variance for λ in the Norton ensemble with the variance for R in the standard NEMD equilibrium ensembles.



Pearson autocorrelations functions for $\eta = r = 0$ in the standard NEMD and Norton ensembles. Left: standard NEMD, Right: Norton.

Shear viscosity: scaling of variance

Scaling of the variance with system size:



NEMD: $\text{Var}_{\mu^0}(R) = O(N^{-1}) \rightarrow$ consistent with spatial CLT.

Dual method: $\text{Var}_{\mu^0,*}(\lambda) = O(N^{-5/3}) \rightarrow$ gain in asymptotic variance increases with system size.

Conclusion

This work:

- General framework to derive dual nonequilibrium dynamics.
- Consistency/promising scaling properties of the approach on simple but realistic systems.
- Class of numerical methods (splitting schemes for dual Langevin dynamics).

Many theoretical questions are opened:

- Well-posedness, existence/uniqueness of steady-state, ergodicity/convergence to equilibrium for the dual dynamics.
- Equivalence of (non)equilibrium ensembles, equivalence of linear responses, Green–Kubo type formulas.
- Numerical analysis: scaling law for $\text{Var}(\lambda)$ / correlation times, error analysis for numerical schemes.

Simulations using Molly: <https://github.com/JuliaMolSim/Molly.jl>

Code available at: <https://github.com/noeblassel/ArticleNorton/>

Preprint: <https://arxiv.org/abs/2305.08224>

Thank you!